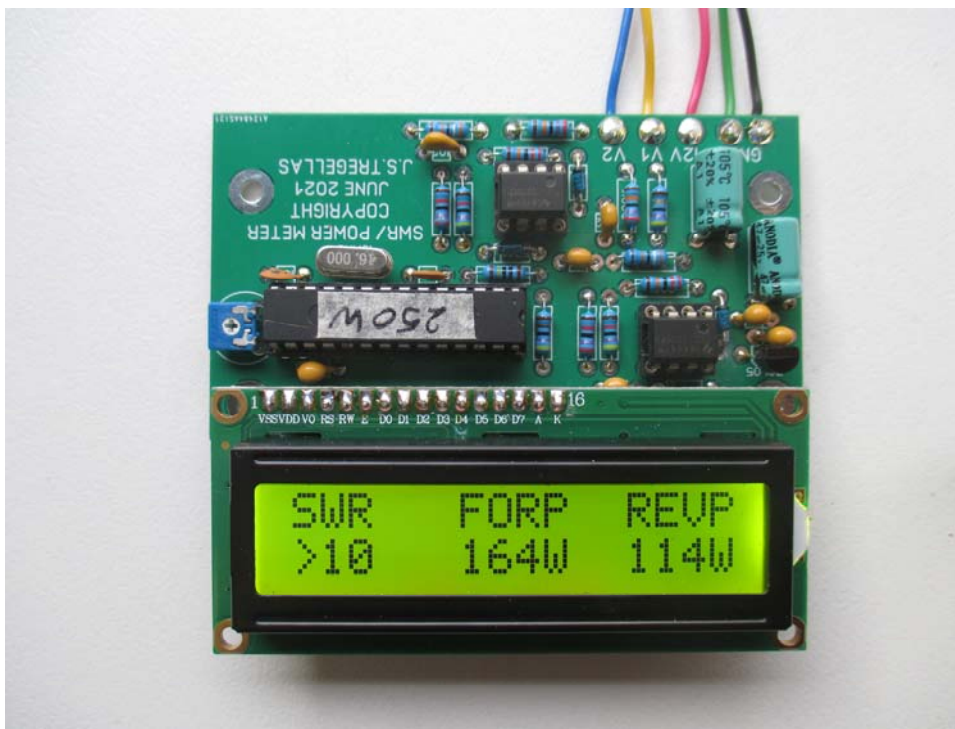
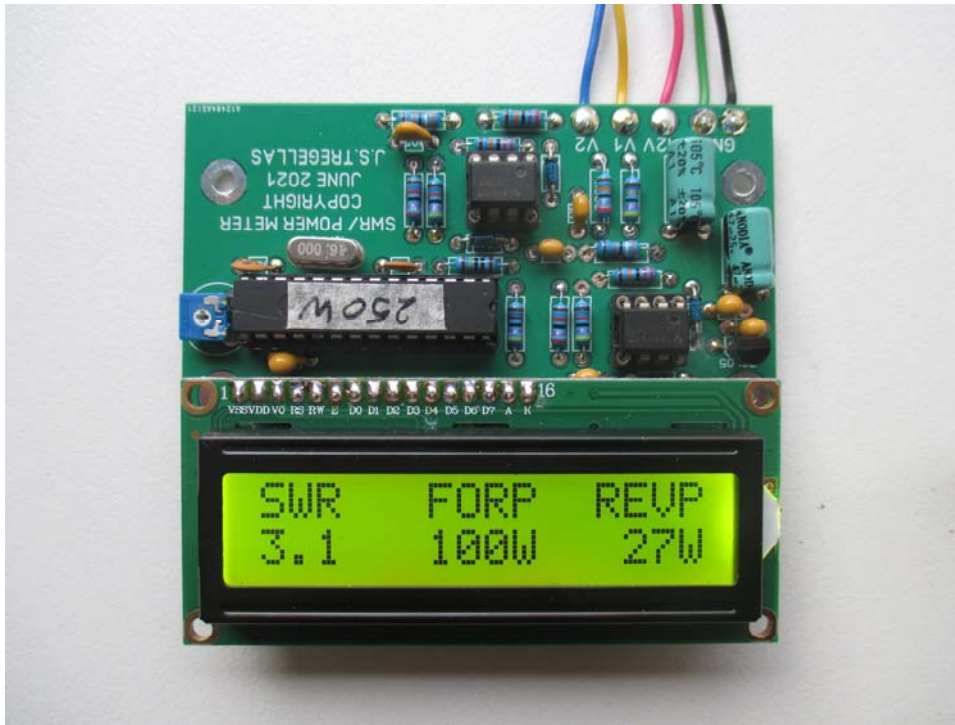
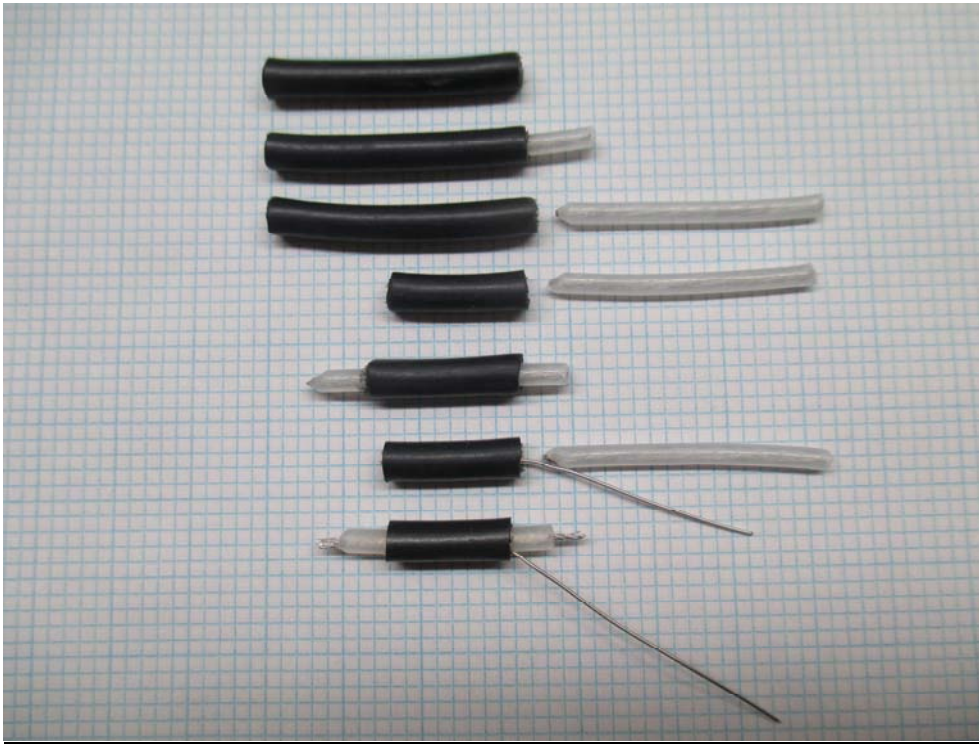


Note the photos show the 250 watt unit , NOT the 1200 watt assembly described within this pamphlet which of course indicates overload at 1200 watts ☺☺







## **A 1200Watt PEP SWR and Power Meter for HF.**

### **Introduction**

For many years, a cheap and accurate digital HF SWR meter has been a pipe dream of several members of the Adelaide Hills Amateur Radio Society, and this article represents a practical realisation of these thoughts. This instrument reliably displays both SWR and the associated instantaneous forward and reverse powers that produce this SWR figure. It works from 1.6 to 55 MHz, accurately displaying powers from QRP levels to 1200 watts, and happily shows PEP for both speech, and for continuous test tones from say a two tone test input. It is built around a Tandem Match or Stockton bridge, the operating theory of which was extensively covered in AR magazine No.4 2021.

### **How It Works**

If the circuit is examined, it will be noted that there are two identical circuit chains which finally feed two A/D converters in the microprocessor (AN0 and AN1 on pins 2 and 3). To keep things simple we will examine only one of these chains under conditions of 1200 watts applied power to the bridge and an SWR of 1.00. Under this special condition, envelope detector D2 and its associated storage capacitor C3 produce maximum dc output (maximum forward power) while detector D1 and C2 produce no dc output because there is no reflected power.

To give maximum detector linearity, the rf applied to these detectors is made as large as possible so that the effects of the diode forward voltage drop are minimised. With an input to the bridge of 1200 watts, the primary current through T1 is 4.89 amps which gives a secondary current of 163.3 ma (turns ratio of 30) which in turn produces 8.164 volts rms or 11.54 volts peak into D2//C3 and causes R5//R6//R7 to dissipate just over one watt.

To reject any rf kicking around the shack but ensure that any modulation peak is not flattened by averaging, a short time constant is used between the detector output and IC1a pin3. This explains why such small values of capacitors are used for C3, C4, and C5. 11.54 volts peak is a bit too close to the top end of the input range of the IC1a op amp (with its 12 volt supply) and so it is scaled back to around 7.14 volts dc by R9/R11.

Under some measurement conditions, one or both of the detectors receive little rf energy. This situation occurs when the total input power to the bridge is small, or when the SWR is low and little rf is fed to the circuits for reflected power. Under these conditions, these detectors are quite badly non linear due to the forward voltage drops of D2/D1. This non linearity is reasonably well corrected by using the same type of diode (D3/D4) in the negative feedback path of IC1a and IC2a--which are essentially voltage followers with a gain of one .

After further scaling by R15 and R16, the 7.14 volts becomes 4.53 volts dc peak at the input of IC1b (pin 5) which in turn is stored by the sample and hold circuit IC1b in C7. C7 and R19 have a long time constant (1 second) which allows the instrument to store the latest modulation peak while at the same time providing a reasonable recovery time after rf signals cease. Of course, 4.53 volts at either of the two microprocessor A/D inputs (pins 2 and 3) represents a power of 1200 watts. Due to the fact that the microprocessor operates from a 5 volt rail, a 1200 watt input will consequently not over range the A/D input, where 5 volts represents the maximum input possible to the A/D converter. The stored values of dc voltage in C7 and C8 are then used by the microprocessor to calculate SWR and forward and reverse power.

### **Building the beast**

The fact that the bridge circuit and the microprocessor are built on two different pcbs allows great flexibility in construction. The preferred construction method is to build the bridge circuit into a separate box, creating a test head which can be wired into any desired place in an antenna system. This test head is remotely connected to the microprocessor and LCD which are then placed in a convenient location for viewing. If you pursue this idea of a separate measurement head, use a two wire screened cable for the interconnection. Of course, both boards can be also built into a single box if desired.

Further flexibility is built in by the way in which the microprocessor board and LCD can be assembled. They can be interconnected as shown in the attached pictures, or with the microprocessor board directly behind the LCD, or with the two boards at right angles. This allows the use of a huge number of enclosures.

Assembly is very straight forward and reference should simply be made to the component overlay drawing. USE IC SOCKETS. **If you are going to place the main board directly behind the LCD, use flexible wire to interconnect the two parts.** This will allow access to the back of the main pcb in the event of any errors.

The only area which may give difficulty is the assembly of the toroids and their associated short lengths of coaxial cable in the measurement bridge. Do not try to bring the woven sheath of the coaxial cable out (which forms a Faraday shield). If you do there is a large chance of soldering heat moving back up the sheath wires during assembly and causing shorts because the central insulation has melted. Life is made much easier by inserting a short length of thin tinned copper wire within the woven sheath to make the ground connection for the Faraday shield. The photo shows the various stages in this process . Cut a length of 34mm from a piece of RG58 coaxial cable. Carefully

push the central conductor out, and sharpen the insulation at one end to a V point using a knife or bench grinder. Cut the remaining insulation and sheath to a length of 18mm. Reinsert the centre conductor into the external insulation and sheath to reform the flattened woven sheath. Remove the central conductor and insert a short length of thin tinned copper wire within the sheath. Now reinsert the central conductor to form the final assembly and then strip both ends of this back by 3mm.

An alternative is to simply place a bare 18mm length of woven sheath over the central coax conductor and ground wire, and then overlay this assembly with heat shrink tube so that the assembly fits snugly and CENTRALLY within the toroid and associated winding.

Finally add the toroid with its 30 turns of 0.4mm diameter wire to this inner assembly. The 30 turns should be evenly distributed around the toroid circumference. Tin both wires from the toroid and add the entire assembly to the pcb. Both toroid and coax cable assemblies should be closely identical (particularly with regard to the toroid winding direction) and **30 turns on the toroid means that the wire should pass through the centre of the toroid 30 times.**

Before placing the completed sensor pcb into the box, make life easy by soldering 40mm lengths of bare copper wire to the five input/output points on the pcb making it ready to connect to the SO239 connectors, and ground and two dc outputs on the DIN connector. Finally note the bent over solder lugs shown in the photos connecting the body of both SO239 connectors to the pcb ground plane.

### Setting the unit to work

Provided the toroids have been accurately wound, there is no calibration needed. Measurement accuracy should be better than about 5% over an extended temperature range because that is the worst case tolerance on the 5 volt supply rail to the microprocessor. This rail voltage represents the full scale output count from the 8 bit analog to digital converters of 255 and hence sets the accuracy of all calculations when an input voltage is compared to it. The only adjustment needed is to set the contrast control for the LCD to produce good visible readings. If desired, calibration can be checked by using one of the 50 ohm dummy loads with attached envelope detector detailed in AR magazine volume 2, 2020. The diagram at the rear of this article shows the dummy load with its envelope detector and all other connections in detail. If a 5% tolerance on power readings is unacceptable, closer tolerance readings may be obtained by changing the value of **both** R11 and R12 upwards or downwards by say one value to 330K or 470K.

The PEP power display which the unit produces is interesting. This instrument displays (RMS) power, which is the product of RMS volts and RMS current. For SSB, the display shows PEP which is the (RMS) power of the highest modulation peaks. For a typical 100 watt PEP SSB transceiver set to produce AM, it will typically show 25 watts for an unmodulated carrier, and 100 watts (PEP) for a 100% modulated carrier (unless downward modulation is used). The power quadruples because the voltage doubles at the modulation peaks relative to that of the unmodulated carrier. For FM, the carrier amplitude is constant and so (RMS) power is displayed.

Note that if the assembly displays equal forward and reverse powers and an SWR of greater than 10 with a dummy load connected instead of the antenna, then the connections to the radio and antenna system are reversed.



## **Diagnostics**

If the assembled unit does not function, first check the obvious things such as the 5 volt supply rail and your soldering (for missed and dry joints, and for solder bridges) . Also check that the chips are in their sockets correctly with no folded under pins. Note the the dc voltage existing at pin 3 of IC1 and IC2 is not published because even the 10 megohm input impedance of a standard DVM will load this high impedance point down excessively. However due to negative feedback, the voltage at pin 2 will match it within a few millivolts. If the LCD displays nothing, check the operation of the microprocessor clock by probing the clock circuit with an oscilloscope and X10 probe. The X10 probe should grasp one lead of a series capacitor of around 4.7pf while the other lead is used to probe the clock circuit. This prevents excessive capacitive loading stopping clock operation. Alternatively, the clock can be checked by listening at 16MHz with a radio receiver with short wire antenna.

Next, disconnect the bridge pcb from the main pcb. The operation of the bridge can be checked by applying rf to it and noting the dc output that occurs at different power levels by referring to table 1 below .Use the dummy load with rectifying diodes as shown on the last page to measure rf power levels.

Finally check the dc levels through the amplifier chain by directly connecting the on board 5 volt supply to IC1 pin3. The dc levels shown below should be present if all is well and a power level of around 640 watts should be indicated. When the same check is done on IC2, the dc voltage levels should be identical but the indicated power will be zero, because the microprocessor software objects violently when the reflected power is greater than the forward power.

**Table 1**

Bridge input power	800W	400W	200W	100W
Bridge DC output	9.2V	6.46V	4.5V	3.12V

**Table 2**

IC1a Pin3	IC1a Pin2	IC1a Pin 1	IC1b Pin 5	IC1b Pin6	IC1bPin5
5.00V	5.00V	5.16V	3.28V	3.28V	3.39

## **Kits**

Initially, kits of parts will be available from the author for \$40 plus postage (email [endsodds@internode.on.net](mailto:endsodds@internode.on.net) for more details). Everything will be supplied except for the enclosure for the main pcb and LCD. This is not supplied because the LCD and main board can be assembled in at least 3 possible ways, and many amateurs may want to build these assemblies into existing enclosures.

Note that the idea behind this project is to provide funds for the Adelaide Hills Amateur Radio Society with all profits going to the club. Watch their website [www.ahars.com.au](http://www.ahars.com.au) for updates.

## **Finally**

My considerable thanks to my good friend Barry Williams VK5BW for his able assistance in this project . His sharp mind and model 4391A and 43 Bird wattmeters kept me honest.....

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## **Parts List- 1200 watt SWR and Power Meter**

### **Resistors and trimpots**

All resistors are 0.5 watt 1% metal film

1@ 47R

6@ 150R

1@ 4K7

2@ 10K

2@ 27K

2@ 47K

2@220K

2@ 240K

2@390K

2@ 1M

1@ 5K,10K or 20K trimpot

### **Capacitors**

Unless otherwise specified all capacitors are 50V

multiplate monolithic types with 0.2 inch lead spacing

2@ 15pf

2@ 100pf

4@ 1nF

3@ 100nF

2@ 1uF

2@ 47uF or 100uF 25V aluminium electrolytic

### **Semiconductors**

1@ 16F873 or 16F683A (software loaded)

2@ LM358 DIL op amps

1@ 78L05 (TO92 pack)

6@ 1N5711 Schottky diodes

1@ 1602A green LCD

### **Plugs and Sockets**

1@ 28 pin DIP socket

2@ 8 pin DIP socket

2@ SO239 panel mount sockets

1@ 5 pin panel mount DIN socket

1@ 5 pin DIN plug

### **Hardware**

2@ pcbs

1@ 16 pin length of 16 pin terminal strip

2@ FT50-43 toroids

1300 mm of 0.4mm diameter enameled copper wire

2@ 34mm lengths of RG58 coaxial cable

100mm length of 0.5mm diameter tinned copper wire

1@ UB5 jiffy box

10@ M3 cheesehead screws 6mm long

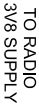
10@ M3 nuts

2@ 3.2mm bore solder tags

1@ 16MHz crystal

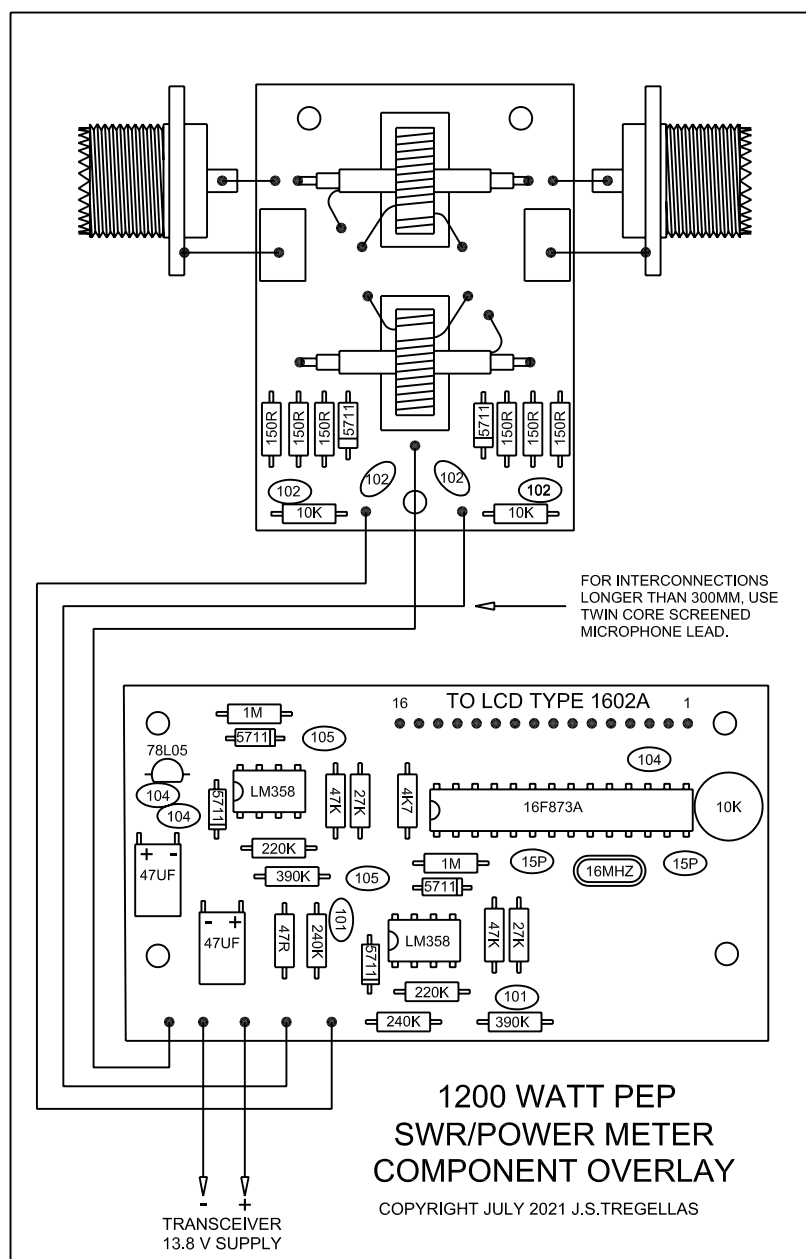
1@ set of instructions

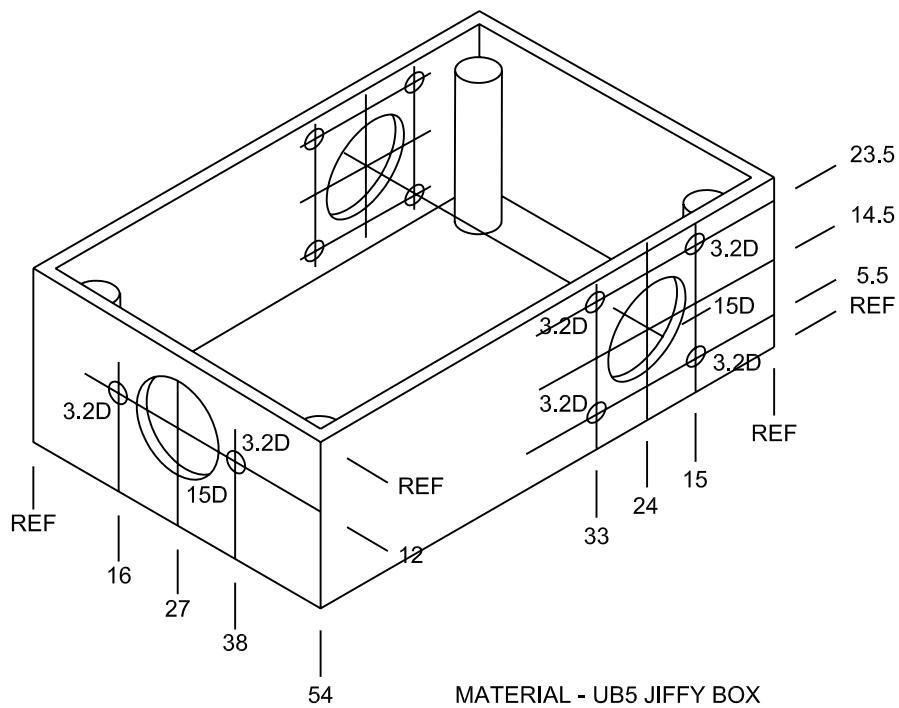
\*\*\*\* Note that it is assumed that the builder will provide the enclosure for the LCD and main pcb.



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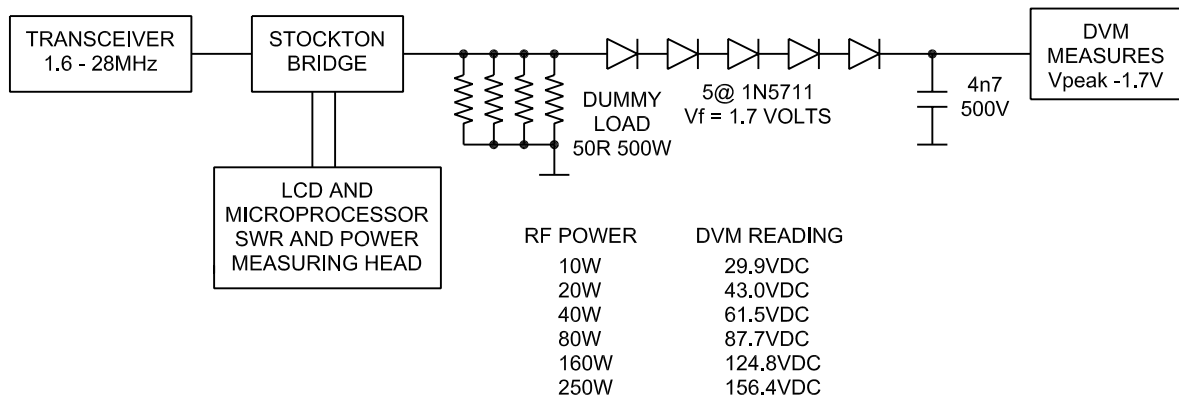






## DRILLING DETAILS FOR REMOTE SENSING HEAD

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## TEST RIG TO CHECK RF POWER LEVEL